

A Moving Mesh Finite Element Method for Modelling Defects in Liquid Crystals

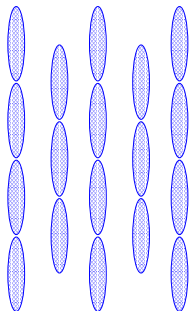
Alison Ramage

Department of Mathematics and Statistics, University of Strathclyde

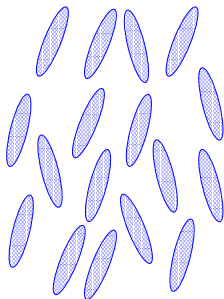


Joint work with Craig MacDonald and John Mackenzie

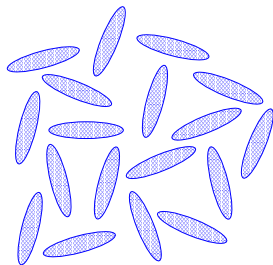
Liquid crystals



solid



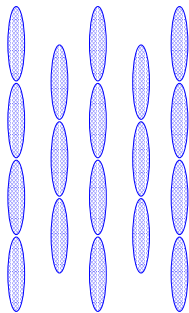
liquid crystal



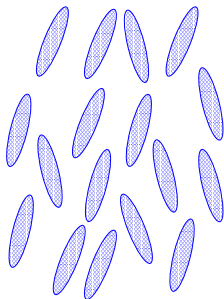
liquid

- Liquid crystals occur between solid crystal and isotropic liquid states.

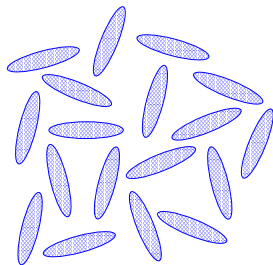
Liquid crystals



solid



liquid crystal



liquid

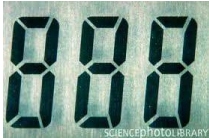
- Liquid crystals occur between solid crystal and isotropic liquid states.
- They may have different **equilibrium** configurations, but naturally prefer states with **minimum** energy.

Liquid Crystal Displays

- **IDEA**: force switching between **stable** states by altering applied voltage, magnetic field, boundary conditions, . . .

Liquid Crystal Displays

- **IDEA:** force switching between **stable** states by altering applied voltage, magnetic field, boundary conditions, . . .
- Used in a wide range of LCDs.



Motivation

- **Defects** in a liquid crystal can arise due to external factors such as applied **electric or magnetic** fields, or the constraining geometry of the liquid crystal cell.

Motivation

- **Defects** in a liquid crystal can arise due to external factors such as applied **electric or magnetic** fields, or the constraining geometry of the liquid crystal cell.
- Understanding the **formation and dynamics** of defects is important in the design and control of liquid crystal devices.

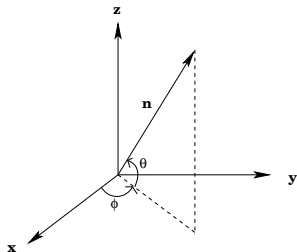
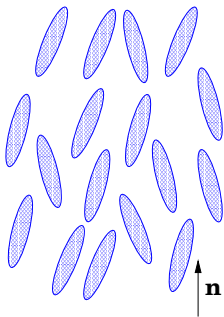
Motivation

- **Defects** in a liquid crystal can arise due to external factors such as applied **electric or magnetic** fields, or the constraining geometry of the liquid crystal cell.
- Understanding the **formation and dynamics** of defects is important in the design and control of liquid crystal devices.
- Defects typically induce distortion over **very small length scales** as compared to the size of the cell: this poses **significant challenges** for standard numerical modelling techniques.

Motivation

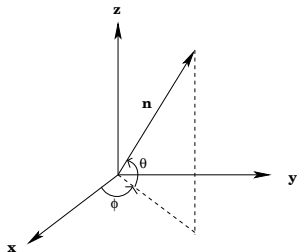
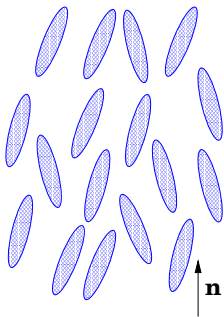
- **Defects** in a liquid crystal can arise due to external factors such as applied **electric or magnetic** fields, or the constraining geometry of the liquid crystal cell.
- Understanding the **formation and dynamics** of defects is important in the design and control of liquid crystal devices.
- Defects typically induce distortion over **very small length scales** as compared to the size of the cell: this poses **significant challenges** for standard numerical modelling techniques.
- In this talk we present a finite-element based **adaptive moving mesh** model for tracking defect movement.

Director-based model



- **Director**: represents average direction of molecular alignment

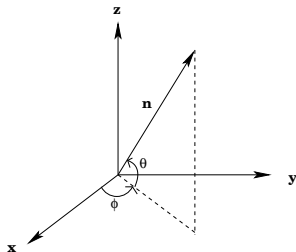
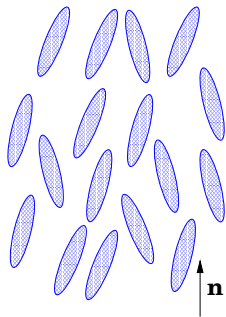
Director-based model



- **Director**: represents average direction of molecular alignment
- Represent using unit vectors with $\mathbf{n} = -\mathbf{n}$:

$$\mathbf{n} = (\cos \theta \cos \phi, \cos \theta \sin \phi, \sin \theta)$$

Director-based model



- **Director**: represents average direction of molecular alignment
- Represent using unit vectors with $\mathbf{n} = -\mathbf{n}$:
$$\mathbf{n} = (\cos \theta \cos \phi, \cos \theta \sin \phi, \sin \theta)$$
- Model with **Leslie-Ericksen** dynamic theory.

Liquid crystal model: Q-tensor theory

- Describe orientation of each molecule by a single vector \mathbf{u} in direction of its main axis.

Liquid crystal model: \mathbf{Q} -tensor theory

- Describe orientation of each molecule by a single vector \mathbf{u} in direction of its main axis.
- Represent **average** orientation by **symmetric** and **traceless** order tensor

$$\mathbf{Q} = \sqrt{\frac{3}{2}} \left\langle \mathbf{u} \otimes \mathbf{u} - \frac{1}{3} \mathbf{I} \right\rangle.$$

Liquid crystal model: Q-tensor theory

- Describe orientation of each molecule by a single vector \mathbf{u} in direction of its main axis.
- Represent **average** orientation by **symmetric** and **traceless** order tensor

$$\mathbf{Q} = \sqrt{\frac{3}{2}} \left\langle \mathbf{u} \otimes \mathbf{u} - \frac{1}{3} \mathbf{I} \right\rangle.$$

- With orthogonal eigenframe $\{\mathbf{l}, \mathbf{m}, \mathbf{n}\}$, write

$$\mathbf{Q} = S \left(\mathbf{n} \otimes \mathbf{n} - \frac{1}{3} \mathbf{I} \right) + T (\mathbf{m} \otimes \mathbf{m} - \mathbf{l} \otimes \mathbf{l})$$

where S , T are **uniaxial** and **biaxial** order parameters.

Liquid crystal model: Q-tensor theory

- Describe orientation of each molecule by a single vector \mathbf{u} in direction of its main axis.
- Represent **average** orientation by **symmetric** and **traceless** order tensor

$$\mathbf{Q} = \sqrt{\frac{3}{2}} \left\langle \mathbf{u} \otimes \mathbf{u} - \frac{1}{3} \mathbf{I} \right\rangle.$$

- With orthogonal eigenframe $\{\mathbf{l}, \mathbf{m}, \mathbf{n}\}$, write

$$\mathbf{Q} = S \left(\mathbf{n} \otimes \mathbf{n} - \frac{1}{3} \mathbf{I} \right) + T (\mathbf{m} \otimes \mathbf{m} - \mathbf{l} \otimes \mathbf{l})$$

where S , T are **uniaxial** and **biaxial** order parameters.

- Consider **uniaxial** molecular distribution ($T = 0$) where \mathbf{n} is the liquid crystal **director**.

Q-tensor representation

- Symmetric traceless tensor Q has five degrees of freedom.

Q-tensor representation

- Symmetric traceless tensor \mathbf{Q} has **five** degrees of freedom.
- Represent \mathbf{Q} using a (non-unique) basis of five linearly-independent tensors, e.g.

$$\mathbf{Q} = \begin{bmatrix} q_1 & q_2 & q_3 \\ q_2 & q_4 & q_5 \\ q_3 & q_5 & -q_1 - q_4 \end{bmatrix}.$$

Q-tensor representation

- Symmetric traceless tensor \mathbf{Q} has **five** degrees of freedom.
- Represent \mathbf{Q} using a (non-unique) basis of five linearly-independent tensors, e.g.

$$\mathbf{Q} = \begin{bmatrix} q_1 & q_2 & q_3 \\ q_2 & q_4 & q_5 \\ q_3 & q_5 & -q_1 - q_4 \end{bmatrix}.$$

- **Five** unknowns for PDE model:

$$q_1, q_2, q_3, q_4, q_5.$$

Q-tensor equations

- Minimise the **free energy**:

$$F = \int_V F_{bulk}(\mathbf{Q}, \nabla \mathbf{Q}) dv + \int_S F_{surface}(\mathbf{Q}) dS$$

$$F_{bulk} = F_{elastic} + F_{thermotropic} + F_{electrostatic}$$

Q-tensor equations

- Minimise the **free energy**:

$$F = \int_V F_{bulk}(\mathbf{Q}, \nabla\mathbf{Q}) dv + \int_S F_{surface}(\mathbf{Q}) dS$$

$$F_{bulk} = F_{elastic} + F_{thermotropic} + F_{electrostatic}$$

- Derive expressions for individual energy contributions in terms of \mathbf{Q} , $\nabla\mathbf{Q}$.

Q-tensor equations

- Minimise the **free energy**:

$$F = \int_V F_{bulk}(\mathbf{Q}, \nabla\mathbf{Q}) dv + \int_S F_{surface}(\mathbf{Q}) dS$$

$$F_{bulk} = F_{elastic} + F_{thermotropic} + F_{electrostatic}$$

- Derive expressions for individual energy contributions in terms of \mathbf{Q} , $\nabla\mathbf{Q}$.
- With **strong anchoring** (Dirichlet boundary conditions), there is no contribution from surface energy.

- Minimise the **free energy**:

$$F = \int_V F_{bulk}(\mathbf{Q}, \nabla\mathbf{Q}) dv + \int_S F_{surface}(\mathbf{Q}) dS$$

$$F_{bulk} = F_{elastic} + F_{thermotropic} + F_{electrostatic}$$

- Derive expressions for individual energy contributions in terms of \mathbf{Q} , $\nabla\mathbf{Q}$.
- With **strong anchoring** (Dirichlet boundary conditions), there is no contribution from surface energy.
- Solutions with **least** energy are physically relevant: solve **Euler-Lagrange** equations.

Bulk energies

- **Elastic** energy: induced by distorting the \mathbf{Q} -tensor in space.

$$F_{elastic} = \frac{1}{2}L_1(\operatorname{div} \mathbf{Q})^2 + \frac{1}{2}L_2|\nabla \times \mathbf{Q}|^2$$

Bulk energies

- **Elastic** energy: induced by distorting the \mathbf{Q} -tensor in space.

$$F_{elastic} = \frac{1}{2}L_1(\text{div } \mathbf{Q})^2 + \frac{1}{2}L_2|\nabla \times \mathbf{Q}|^2$$

- **Thermotropic** energy: potential function which dictates which preferred state (uniaxial, biaxial or isotropic).

$$F_{thermotropic} = \frac{1}{2}A(T - T^*) \text{tr } \mathbf{Q}^2 - \frac{\sqrt{6}}{3}B \text{tr } \mathbf{Q}^3 + \frac{1}{4}C(\text{tr } \mathbf{Q}^2)^2$$

Bulk energies

- **Elastic** energy: induced by distorting the \mathbf{Q} -tensor in space.

$$F_{elastic} = \frac{1}{2}L_1(\text{div } \mathbf{Q})^2 + \frac{1}{2}L_2|\nabla \times \mathbf{Q}|^2$$

- **Thermotropic** energy: potential function which dictates which preferred state (uniaxial, biaxial or isotropic).

$$F_{thermotropic} = \frac{1}{2}A(T - T^*) \text{tr } \mathbf{Q}^2 - \frac{\sqrt{6}}{3}B \text{tr } \mathbf{Q}^3 + \frac{1}{4}C(\text{tr } \mathbf{Q}^2)^2$$

- **Electrostatic** energy: due to an applied electric field \mathbf{E} (electric potential U with $\mathbf{E} = -\nabla U$).

$$F_{electrostatic} = -\frac{1}{2}\epsilon_0\mathbf{E} \cdot \epsilon\mathbf{E} - (\bar{\epsilon} \text{div } \mathbf{Q}) \cdot \mathbf{E}$$

Derivation of time-dependent PDEs

- Use a **dissipation function** with viscosity coefficient ν .

$$\mathcal{D} = \frac{\nu}{2} \text{tr} \left[\left(\frac{\partial \mathbf{Q}}{\partial t} \right)^2 \right] = \nu (\dot{q}_1 \dot{q}_4 + \dot{q}_1^2 + \dot{q}_2^2 + \dot{q}_3^2 + \dot{q}_4^2 + \dot{q}_5^2)$$

Derivation of time-dependent PDEs

- Use a **dissipation function** with viscosity coefficient ν .

$$\mathcal{D} = \frac{\nu}{2} \text{tr} \left[\left(\frac{\partial \mathbf{Q}}{\partial t} \right)^2 \right] = \nu (\dot{q}_1 \dot{q}_4 + \dot{q}_1^2 + \dot{q}_2^2 + \dot{q}_3^2 + \dot{q}_4^2 + \dot{q}_5^2)$$

- Obtain **Q**-tensor PDEs (for $i = 1, \dots, 5$ and $j = 1, 2, 3$):

$$\frac{\partial \mathcal{D}}{\partial \dot{q}_i} = \nabla \cdot \hat{\mathbf{r}}_i - \hat{f}_i$$

$$(\hat{\mathbf{r}}_i)_j = \frac{\partial F_{bulk}}{\partial q_{i,j}}, \quad q_{i,j} = \frac{\partial q_i}{\partial x_j}, \quad \hat{f}_i = \frac{\partial F_{bulk}}{\partial q_i}$$

Derivation of time-dependent PDEs

- Use a **dissipation function** with viscosity coefficient ν .

$$\mathcal{D} = \frac{\nu}{2} \text{tr} \left[\left(\frac{\partial \mathbf{Q}}{\partial t} \right)^2 \right] = \nu (\dot{q}_1 \dot{q}_4 + \dot{q}_1^2 + \dot{q}_2^2 + \dot{q}_3^2 + \dot{q}_4^2 + \dot{q}_5^2)$$

- Obtain **Q**-tensor PDEs (for $i = 1, \dots, 5$ and $j = 1, 2, 3$):

$$\frac{\partial \mathcal{D}}{\partial \dot{q}_i} = \nabla \cdot \hat{\Gamma}_i - \hat{f}_i$$

$$(\hat{\Gamma}_i)_j = \frac{\partial F_{bulk}}{\partial q_{i,j}}, \quad q_{i,j} = \frac{\partial q_i}{\partial x_j}, \quad \hat{f}_i = \frac{\partial F_{bulk}}{\partial q_i}$$

- Combining equations and manipulating terms gives

$$\frac{\partial q_i}{\partial t} = \nabla \cdot \Gamma_i - f_i, \quad i = 1, \dots, 5.$$

Coupling with electric field

- Additional unknown U such that $\mathbf{E} = -\nabla U$.

Coupling with electric field

- Additional unknown U such that $\mathbf{E} = -\nabla U$.
- Assuming no free charges, solve the **Maxwell equation**
 $\nabla \cdot \mathbf{D} = 0$, electric displacement \mathbf{D} .

Coupling with electric field

- Additional unknown U such that $\mathbf{E} = -\nabla U$.
- Assuming no free charges, solve the **Maxwell equation**
 $\nabla \cdot \mathbf{D} = 0$, electric displacement \mathbf{D} .

SUMMARY

- Final time-dependent physical PDEs (**PPDEs**) are

$$\frac{\partial q_i}{\partial t} = \nabla \cdot \mathbf{\Gamma}_i - f_i \quad i = 1, \dots, 5$$

$$\nabla \cdot \mathbf{D} = 0$$

- 6 PDEs in 6 unknowns $(q_1, q_2, q_3, q_4, q_5, U)$

Adaptive finite element methods

- Three common forms of grid adaptivity in finite elements:
 - ***h*-refinement**: initially uniform mesh is locally **coarsened or refined** by inclusion or deletion of mesh points, normally based on *a posteriori* error estimates
 - ***p*-refinement**: **order of local polynomial approximation** is increased or decreased in accordance with solution error
 - ***r*-refinement**: original mesh points are **moved** to areas where high resolution is needed

Adaptive finite element methods

- Three common forms of grid adaptivity in finite elements:
 - ***h*-refinement**: initially uniform mesh is locally **coarsened or refined** by inclusion or deletion of mesh points, normally based on *a posteriori* error estimates
 - ***p*-refinement**: **order of local polynomial approximation** is increased or decreased in accordance with solution error
 - ***r*-refinement**: original mesh points are **moved** to areas where high resolution is needed
- Advantages of moving meshes:
 - retaining **fixed** number of mesh points and connectivity;
 - **interpolation** from old to new mesh unnecessary for time-dependent problems.

Adaptive finite element methods

- Three common forms of grid adaptivity in finite elements:
 - ***h*-refinement**: initially uniform mesh is locally **coarsened or refined** by inclusion or deletion of mesh points, normally based on *a posteriori* error estimates
 - ***p*-refinement**: **order of local polynomial approximation** is increased or decreased in accordance with solution error
 - ***r*-refinement**: original mesh points are **moved** to areas where high resolution is needed
- Advantages of moving meshes:
 - retaining **fixed** number of mesh points and connectivity;
 - **interpolation** from old to new mesh unnecessary for time-dependent problems.
- Focus here on **Moving Mesh PDE** model.

Adapt PPDEs for mesh movement

- **Physical** domain Ω , **computational** domain Ω_c .

Adapt PPDEs for mesh movement

- **Physical** domain Ω , **computational** domain Ω_c .
- Bijective mappings $\mathcal{A}_t : \Omega_c \rightarrow \Omega$ map $\xi = (\xi, \eta) \in \Omega_c$ to $\mathbf{x} = (x, y) \in \Omega$:

$$\mathbf{x}(\xi, t) = \mathcal{A}_t(\xi) .$$

Adapt PPDEs for mesh movement

- **Physical** domain Ω , **computational** domain Ω_c .
- Bijective mappings $\mathcal{A}_t : \Omega_c \rightarrow \Omega$ map $\xi = (\xi, \eta) \in \Omega_c$ to $\mathbf{x} = (x, y) \in \Omega$:

$$\mathbf{x}(\xi, t) = \mathcal{A}_t(\xi) .$$

- Define **mesh velocity**

$$\dot{\mathbf{x}}(\mathbf{x}, t) = \left. \frac{\partial \mathbf{x}}{\partial t} \right|_{\xi} (\mathcal{A}_t^{-1}(\mathbf{x}))$$

and apply the Chain Rule to get

$$\left. \frac{\partial q}{\partial t} \right|_{\xi} = \left. \frac{\partial q}{\partial t} \right|_{\mathbf{x}} + \dot{\mathbf{x}} \cdot \nabla q .$$

Adapt PPDEs for mesh movement

- **Physical** domain Ω , **computational** domain Ω_c .
- Bijective mappings $\mathcal{A}_t : \Omega_c \rightarrow \Omega$ map $\xi = (\xi, \eta) \in \Omega_c$ to $\mathbf{x} = (x, y) \in \Omega$:

$$\mathbf{x}(\xi, t) = \mathcal{A}_t(\xi) .$$

- Define **mesh velocity**

$$\dot{\mathbf{x}}(\mathbf{x}, t) = \left. \frac{\partial \mathbf{x}}{\partial t} \right|_{\xi} (\mathcal{A}_t^{-1}(\mathbf{x}))$$

and apply the Chain Rule to get

$$\left. \frac{\partial q}{\partial t} \right|_{\xi} = \left. \frac{\partial q}{\partial t} \right|_{\mathbf{x}} + \dot{\mathbf{x}} \cdot \nabla q .$$

- Additional **convection-like** term due to the mesh movement.

Finite elements for the physical PDEs

- Final set of six coupled PDEs ($i = 1, \dots, 5$):

$$\left. \frac{\partial q_i}{\partial t} \right|_{\xi} - \dot{\mathbf{x}} \cdot \nabla q = \nabla \cdot \Gamma_i - f_i, \quad \nabla \cdot \mathbf{D} = 0$$

Finite elements for the physical PDEs

- Final set of six coupled PDEs ($i = 1, \dots, 5$):

$$\left. \frac{\partial q_i}{\partial t} \right|_{\xi} - \dot{\mathbf{x}} \cdot \nabla q = \nabla \cdot \Gamma_i - f_i, \quad \nabla \cdot \mathbf{D} = 0$$

- Find $q_{ih}(t)$, U_h such that for test functions v_h

$$\frac{d}{dt} \int_{\Omega} q_{ih} v_h \, d\mathbf{x} - \int_{\Omega} (\nabla \cdot (\dot{\mathbf{x}} q_{ih})) v_h \, d\mathbf{x} = \int_{\Omega} \Gamma_{ih} \cdot \nabla v_h \, d\mathbf{x} - \int_{\Omega} f_{ih} v_h \, d\mathbf{x},$$
$$\int_{\Omega} \mathbf{D}_h \cdot \nabla v_h \, d\mathbf{x} = 0.$$

Finite elements for the physical PDEs

- Final set of six coupled PDEs ($i = 1, \dots, 5$):

$$\left. \frac{\partial q_i}{\partial t} \right|_{\xi} - \dot{\mathbf{x}} \cdot \nabla q = \nabla \cdot \Gamma_i - f_i, \quad \nabla \cdot \mathbf{D} = 0$$

- Find $q_{ih}(t)$, U_h such that for test functions v_h

$$\frac{d}{dt} \int_{\Omega} q_{ih} v_h \, d\mathbf{x} - \int_{\Omega} (\nabla \cdot (\dot{\mathbf{x}} q_{ih})) v_h \, d\mathbf{x} = \int_{\Omega} \Gamma_{ih} \cdot \nabla v_h \, d\mathbf{x} - \int_{\Omega} f_{ih} v_h \, d\mathbf{x},$$
$$\int_{\Omega} \mathbf{D}_h \cdot \nabla v_h \, d\mathbf{x} = 0.$$

- Non-linear differential algebraic system ($i = 1, \dots, 5$)

$$\frac{d}{dt}(M(t)\mathbf{q}_i(t)) = \mathbf{G}_i(t, \mathbf{q}_i(t), \mathbf{u}(t)), \quad \mathbf{C}(\mathbf{q}_i(t), \mathbf{u}(t)) = \mathbf{0}.$$

Moving Mesh PDEs

- Avoid mesh crossings by evolving inverse mapping

$$\mathcal{A}_t^{-1}(\mathbf{x}) = \boldsymbol{\xi}(\mathbf{x}, t).$$

Moving Mesh PDEs

- Avoid mesh crossings by evolving inverse mapping

$$\mathcal{A}_t^{-1}(\mathbf{x}) = \boldsymbol{\xi}(\mathbf{x}, t).$$

- Choose mapping $\boldsymbol{\xi}(\mathbf{x})$ for a fixed t to minimise

$$I[\boldsymbol{\xi}] = \frac{1}{2} \int_{\Omega_t} [(\nabla \boldsymbol{\xi})^T \mathbf{G}^{-1}(\nabla \boldsymbol{\xi}) + (\nabla \boldsymbol{\eta})^T \mathbf{G}^{-1}(\nabla \boldsymbol{\eta})] \, d\mathbf{x}$$

with 2×2 symmetric positive definite **monitor matrix** \mathbf{G} .

Moving Mesh PDEs

- Avoid mesh crossings by evolving inverse mapping

$$\mathcal{A}_t^{-1}(\mathbf{x}) = \boldsymbol{\xi}(\mathbf{x}, t).$$

- Choose mapping $\boldsymbol{\xi}(\mathbf{x})$ for a fixed t to minimise

$$I[\boldsymbol{\xi}] = \frac{1}{2} \int_{\Omega_t} [(\nabla \boldsymbol{\xi})^T G^{-1}(\nabla \boldsymbol{\xi}) + (\nabla \eta)^T G^{-1}(\nabla \eta)] dx$$

with 2×2 symmetric positive definite **monitor matrix** G .

- For robustness, evolve mesh via **gradient flow** equations

$$\frac{\partial \boldsymbol{\xi}}{\partial t} = \frac{P}{\tau} \nabla \cdot (G^{-1} \nabla \boldsymbol{\xi}), \quad \frac{\partial \eta}{\partial t} = \frac{P}{\tau} \nabla \cdot (G^{-1} \nabla \eta).$$

Moving Mesh PDEs

- Avoid mesh crossings by evolving inverse mapping

$$\mathcal{A}_t^{-1}(\mathbf{x}) = \boldsymbol{\xi}(\mathbf{x}, t).$$

- Choose mapping $\boldsymbol{\xi}(\mathbf{x})$ for a fixed t to minimise

$$I[\boldsymbol{\xi}] = \frac{1}{2} \int_{\Omega_t} [(\nabla \boldsymbol{\xi})^T G^{-1}(\nabla \boldsymbol{\xi}) + (\nabla \eta)^T G^{-1}(\nabla \eta)] d\mathbf{x}$$

with 2×2 symmetric positive definite **monitor matrix** G .

- For robustness, evolve mesh via **gradient flow** equations

$$\frac{\partial \boldsymbol{\xi}}{\partial t} = \frac{P}{\tau} \nabla \cdot (G^{-1} \nabla \boldsymbol{\xi}), \quad \frac{\partial \eta}{\partial t} = \frac{P}{\tau} \nabla \cdot (G^{-1} \nabla \eta).$$

- User-specified parameters:

- positive temporal smoothing parameter τ ,
- positive function spatial balancing parameter $P(\mathbf{x}, t)$.

Final form of MMPDE

- Use **monitor function** $w(\mathbf{x}, t)$ with **Winslow** monitor matrix

$$G = \begin{bmatrix} w & 0 \\ 0 & w \end{bmatrix}.$$

Final form of MMPDE

- Use **monitor function** $w(\mathbf{x}, t)$ with **Winslow** monitor matrix

$$G = \begin{bmatrix} w & 0 \\ 0 & w \end{bmatrix}.$$

- In practice, interchange variable roles in MMPDE to obtain

$$\tau \frac{\partial \mathbf{x}}{\partial t} = P(ax_{\xi\xi} + bx_{\xi\eta} + cx_{\eta\eta} + dx_{\xi} + ex_{\eta})$$

$$a = \frac{1}{w} \frac{x_{\eta}^2 + y_{\eta}^2}{J^2}, \quad b = -\frac{2}{w} \frac{(x_{\xi}x_{\eta} + y_{\xi}y_{\eta})}{J^2}, \quad c = \frac{1}{w} \frac{x_{\xi}^2 + y_{\xi}^2}{J^2},$$

$$d = \frac{1}{(wJ)^2} [w_{\xi}(x_{\eta}^2 + y_{\eta}^2) - w_{\eta}(x_{\xi}x_{\eta} + y_{\xi}y_{\eta})],$$

$$e = \frac{1}{(wJ)^2} [-w_{\xi}(x_{\xi}x_{\eta} + y_{\xi}y_{\eta}) + w_{\eta}(x_{\xi}^2 + y_{\xi}^2)].$$

Additional details for MMPDE

- **Boundary conditions** obtained using a 1D MMPDE.

Additional details for MMPDE

- **Boundary conditions** obtained using a 1D MMPDE.
- Discretise in space using **linear** finite elements.
- Discretise in time using a **backward Euler** scheme.

Additional details for MMPDE

- **Boundary conditions** obtained using a 1D MMPDE.
- Discretise in space using **linear** finite elements.
- Discretise in time using a **backward Euler** scheme.
- To avoid solving nonlinear algebraic systems, at $t = t^{n+1}$ evaluate coefficients a, b, c, d, e at the time $t = t^n$.

Additional details for MMPDE

- **Boundary conditions** obtained using a 1D MMPDE.
- Discretise in space using **linear** finite elements.
- Discretise in time using a **backward Euler** scheme.
- To avoid solving nonlinear algebraic systems, at $t = t^{n+1}$ evaluate coefficients a, b, c, d, e at the time $t = t^n$.
- Solve resulting linear systems using iterative method **BiCGSTAB** with **Incomplete LU** preconditioner.

Additional details for MMPDE

- **Boundary conditions** obtained using a 1D MMPDE.
- Discretise in space using **linear** finite elements.
- Discretise in time using a **backward Euler** scheme.
- To avoid solving nonlinear algebraic systems, at $t = t^{n+1}$ evaluate coefficients a, b, c, d, e at the time $t = t^n$.
- Solve resulting linear systems using iterative method **BiCGSTAB** with **Incomplete LU** preconditioner.
- **Adaptive time-stepping** based on computed solutions of PPDEs and MMPDE.

Overview of full algorithm

Set an initial uniform mesh Δ_N^0 . Set the initial guess \mathbf{q}_i^0 .

Select an initial Δt^0 . Set $n = 0$.

while ($t^n < t^{\max}$);

 Evaluate monitor function at time t^n .

 Integrate **MMPDE** forward in time to obtain new grid Δ_N^{n+1} .

 Integrate **PPDEs** forward using SDIRK2 to obtain $\mathbf{q}_i^{n+1}, \mathbf{u}^{n+1}$.

$n := n + 1$.

end while.

Choosing the monitor function

- Consider three different forms of monitor function:
 - **AL**. Based on a measure of the **arc-length** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \left(1 + |\nabla \mathcal{T}(\mathbf{x}, t)|^2\right)^{\frac{1}{2}}$$

Choosing the monitor function

- Consider three different forms of monitor function:
 - **AL**. Based on a measure of the **arc-length** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \left(1 + |\nabla\mathcal{T}(\mathbf{x}, t)|^2\right)^{\frac{1}{2}}$$

- **BM1**. Based on **first-order partial derivatives** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \alpha(\mathbf{x}, t) + |\nabla\mathcal{T}(\mathbf{x}, t)|^{\frac{1}{m}}$$

Choosing the monitor function

- Consider three different forms of monitor function:
 - **AL**. Based on a measure of the **arc-length** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \left(1 + |\nabla\mathcal{T}(\mathbf{x}, t)|^2\right)^{\frac{1}{2}}$$

- **BM1**. Based on **first-order partial derivatives** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \alpha(\mathbf{x}, t) + |\nabla\mathcal{T}(\mathbf{x}, t)|^{\frac{1}{m}}$$

- **BM2**. Based on **second-order partial derivatives** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \alpha(\mathbf{x}, t) + \left(\sqrt{\left(\frac{\partial^2\mathcal{T}}{\partial x^2}\right)^2 + 2\left(\frac{\partial^2\mathcal{T}}{\partial x\partial y}\right)^2 + \left(\frac{\partial^2\mathcal{T}}{\partial y^2}\right)^2}\right)^{\frac{1}{m}}$$

Choosing the monitor function

- Consider three different forms of monitor function:

- **AL**. Based on a measure of the **arc-length** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \left(1 + |\nabla\mathcal{T}(\mathbf{x}, t)|^2\right)^{\frac{1}{2}}$$

- **BM1**. Based on **first-order partial derivatives** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \alpha(\mathbf{x}, t) + |\nabla\mathcal{T}(\mathbf{x}, t)|^{\frac{1}{m}}$$

- **BM2**. Based on **second-order partial derivatives** of \mathcal{T} :

$$w(\mathcal{T}(\mathbf{x}, t)) = \alpha(\mathbf{x}, t) + \left(\sqrt{\left(\frac{\partial^2\mathcal{T}}{\partial x^2}\right)^2 + 2\left(\frac{\partial^2\mathcal{T}}{\partial x\partial y}\right)^2 + \left(\frac{\partial^2\mathcal{T}}{\partial y^2}\right)^2}\right)^{\frac{1}{m}}$$

- Scaling parameters α and m regulate **mesh clustering**.

Choosing the input function

- Consider two different forms of input function:
 - **Scalar order parameter**. Based on the trace of \mathbf{Q}^2

$$\mathcal{T}(\mathbf{x}, t) = \text{tr}(\mathbf{Q}^2)$$

as $\text{tr}(\mathbf{Q}^2) = S^2$ for uniaxial state with order parameter S .

Choosing the input function

- Consider two different forms of input function:
 - **Scalar order parameter**. Based on the trace of \mathbf{Q}^2

$$\mathcal{T}(\mathbf{x}, t) = \text{tr}(\mathbf{Q}^2)$$

as $\text{tr}(\mathbf{Q}^2) = S^2$ for uniaxial state with order parameter S .

- **Biaxiality**. Based on a direct invariant measure of biaxiality

$$\mathcal{T}(\mathbf{x}, t) = \left[1 - \frac{6 \text{tr}(\mathbf{Q}^3)^2}{\text{tr}(\mathbf{Q}^2)^3} \right]^{\frac{1}{2}}$$

taking values ranging from 0 (uniaxial) to 1 (fully biaxial).

Choosing the input function

- Consider two different forms of input function:
 - **Scalar order parameter**. Based on the trace of \mathbf{Q}^2

$$\mathcal{T}(\mathbf{x}, t) = \text{tr}(\mathbf{Q}^2)$$

as $\text{tr}(\mathbf{Q}^2) = S^2$ for uniaxial state with order parameter S .

- **Biaxiality**. Based on a direct invariant measure of biaxiality

$$\mathcal{T}(\mathbf{x}, t) = \left[1 - \frac{6 \text{tr}(\mathbf{Q}^3)^2}{\text{tr}(\mathbf{Q}^2)^3} \right]^{\frac{1}{2}}$$

taking values ranging from 0 (uniaxial) to 1 (fully biaxial).

- Both have extrema at the centre of a defect and **vary rapidly** in the immediate neighbourhood of the defect centre.

Numerical experiments

- PPDEs **non-dimensionalised** with respect to lengths and energies.

Numerical experiments

- PPDEs **non-dimensionalised** with respect to lengths and energies.
- Use **quadratic** triangular finite elements for PPDEs, **linear** finite elements for MMPDE.

Numerical experiments

- PPDEs **non-dimensionalised** with respect to lengths and energies.
- Use **quadratic** triangular finite elements for PPDEs, **linear** finite elements for MMPDE.
- Monitor/input function combinations:

Method name	AL	BM1a	BM1b	BM2b
Monitor function	AL	BM1	BM1	BM2
Input function	$\text{tr}(\mathbf{Q}^2)$	$\text{tr}(\mathbf{Q}^2)$	biaxiality	biaxiality

Numerical experiments

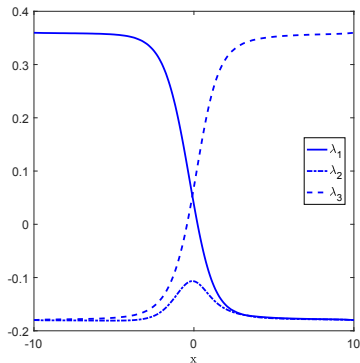
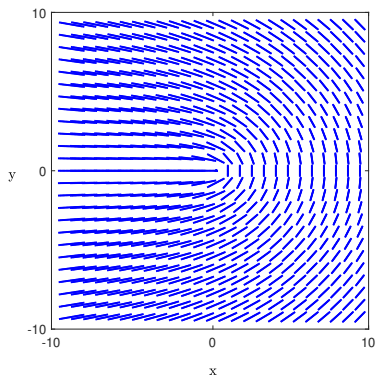
- PPDEs **non-dimensionalised** with respect to lengths and energies.
- Use **quadratic** triangular finite elements for PPDEs, **linear** finite elements for MMPDE.
- Monitor/input function combinations:

Method name	AL	BM1a	BM1b	BM2b
Monitor function	AL	BM1	BM1	BM2
Input function	$\text{tr}(\mathbf{Q}^2)$	$\text{tr}(\mathbf{Q}^2)$	biaxiality	biaxiality

- All experiments carried out in MATLAB.

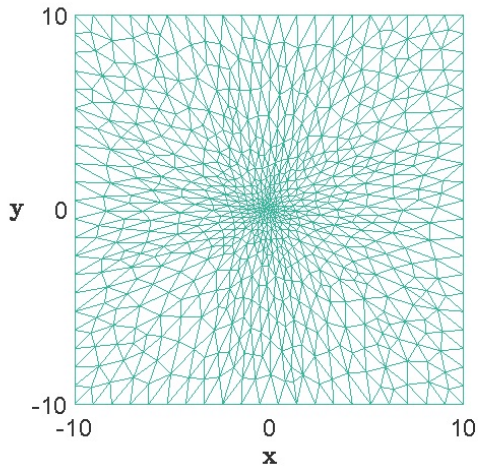
Test problem 1: stationary defect

- Director field of 1/2 defect and eigenvalue exchange along the line $y = 0$.



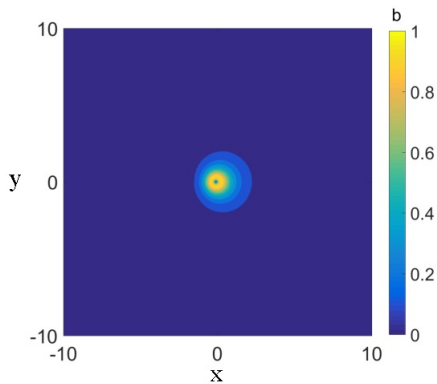
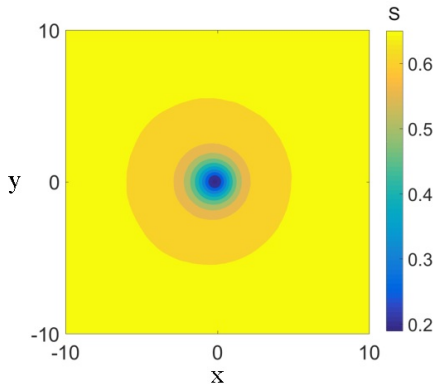
Typical adapted grid

- Sample adapted grid with 1388 quadratic elements.



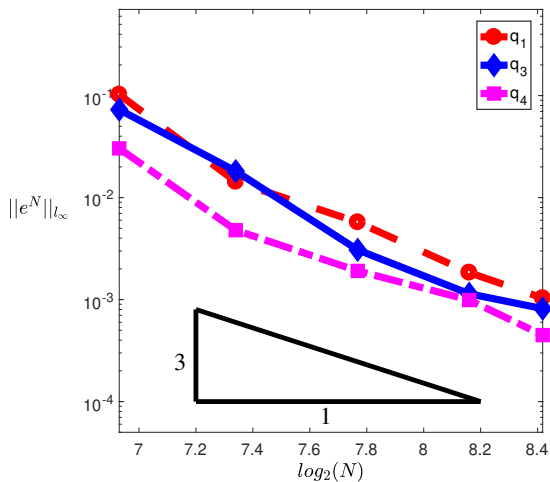
Typical solutions

- Scalar order parameter S (left) and biaxiality (right).



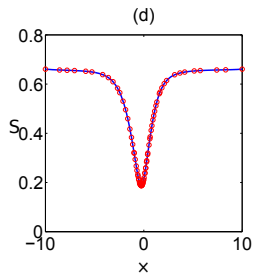
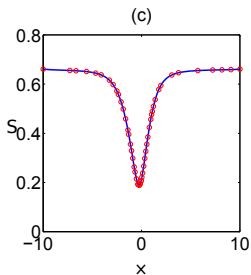
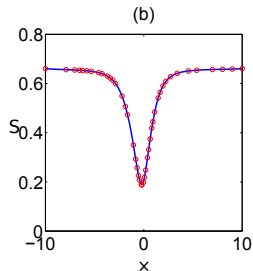
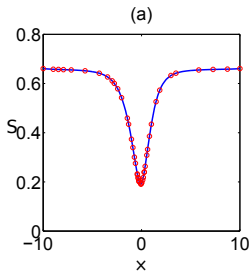
Estimated rate of spatial convergence

- l_∞ error compared with reference solution is $O(N^{-3})$.



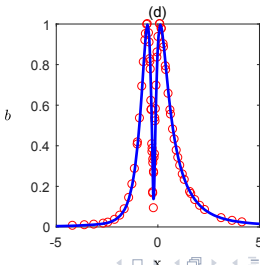
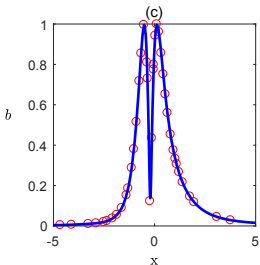
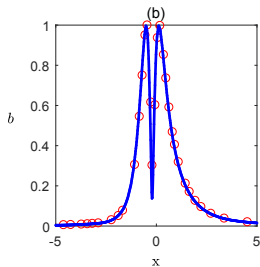
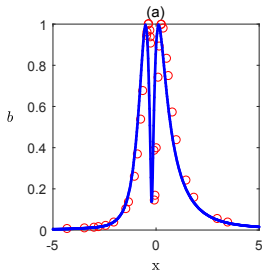
Scalar order parameter along line $y = 0$

- (a) AL; (b) BM1a; (c) BM1b; (d) BM2b



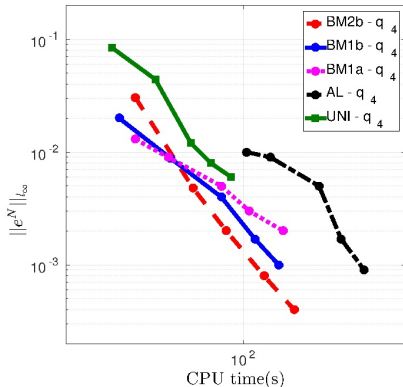
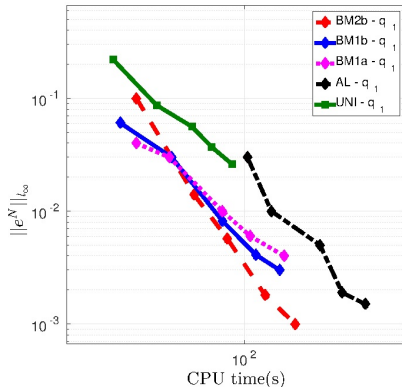
Biaxiality along line $y = 0$

- (a) AL; (b) BM1a; (c) BM1b; (d) BM2b



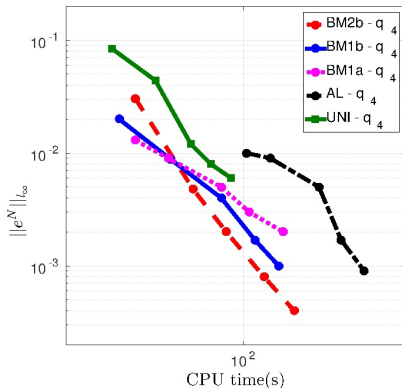
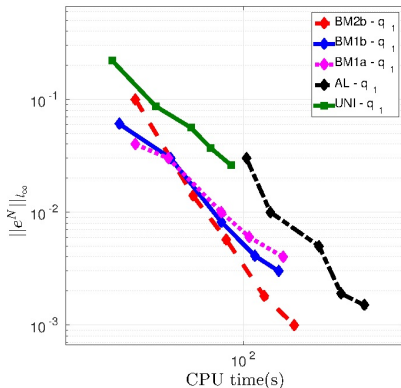
Comparing computational costs

- CPU time versus l_∞ error for different grid sizes.



Comparing computational costs

- CPU time versus l_∞ error for different grid sizes.



- **BM2b** established as combination of choice.

Test problem 2: 2D Pi-cell

- Two-dimensional **Pi-cell** geometry.

Zhang, Chung, Wang and Bos, *Liquid Crystals* 34(2), 2007

Test problem 2: 2D Pi-cell

- Two-dimensional **Pi-cell** geometry.
Zhang, Chung, Wang and Bos, *Liquid Crystals* 34(2), 2007
- Electric field applied parallel to the cell thickness at time $t = 0$.

Test problem 2: 2D Pi-cell

- Two-dimensional **Pi-cell** geometry.
Zhang, Chung, Wang and Bos, *Liquid Crystals* 34(2), 2007
- Electric field applied parallel to the cell thickness at time $t = 0$.
- Inhomogeneous transition mediated by the nucleation of **defect pairs** moving and annihilating each other.

Test problem 2: 2D Pi-cell

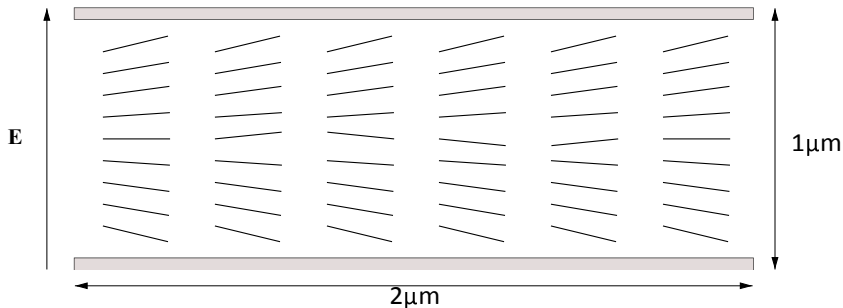
- Two-dimensional **Pi-cell** geometry.
Zhang, Chung, Wang and Bos, *Liquid Crystals* 34(2), 2007
- Electric field applied parallel to the cell thickness at time $t = 0$.
- Inhomogeneous transition mediated by the nucleation of **defect pairs** moving and annihilating each other.
- Initial director angle across cell centre follows $\sin(2\pi x/p)$ for cell width p .

Test problem 2: 2D Pi-cell

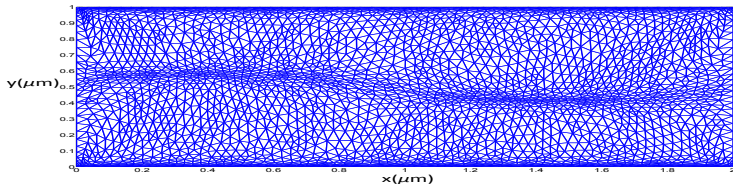
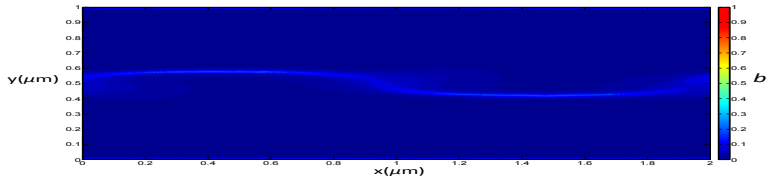
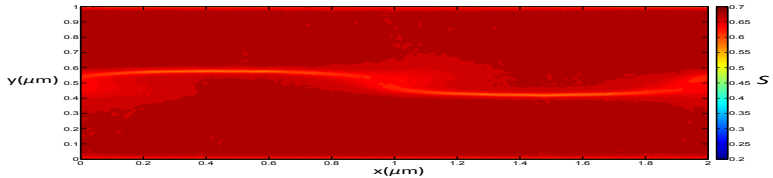
- Two-dimensional **Pi-cell** geometry.
Zhang, Chung, Wang and Bos, *Liquid Crystals* 34(2), 2007
- Electric field applied parallel to the cell thickness at time $t = 0$.
- Inhomogeneous transition mediated by the nucleation of **defect pairs** moving and annihilating each other.
- Initial director angle across cell centre follows $\sin(2\pi x/p)$ for cell width p .
- Perturbation fixed only at $t = 0$ for one time step, but introduces **solution gradients** in two dimensions.

Pi-cell geometry

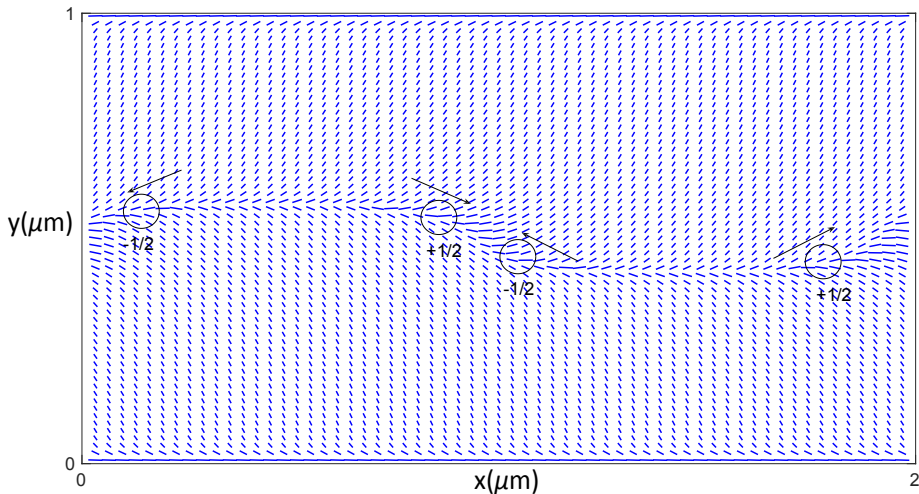
- Pre-tilt angle $\theta = \pm 6^\circ$ at boundaries.
- Electric field strength $18V\mu\text{m}^{-1}$.



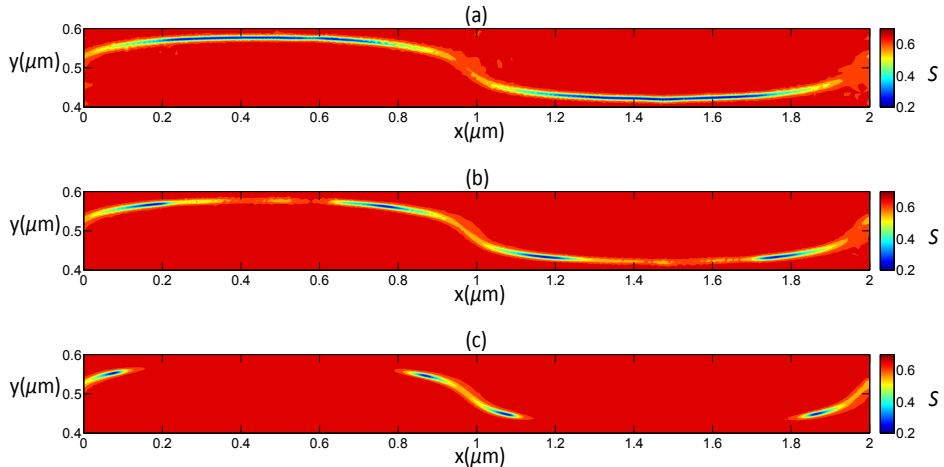
S , biaxiality and mesh after $12\mu s$



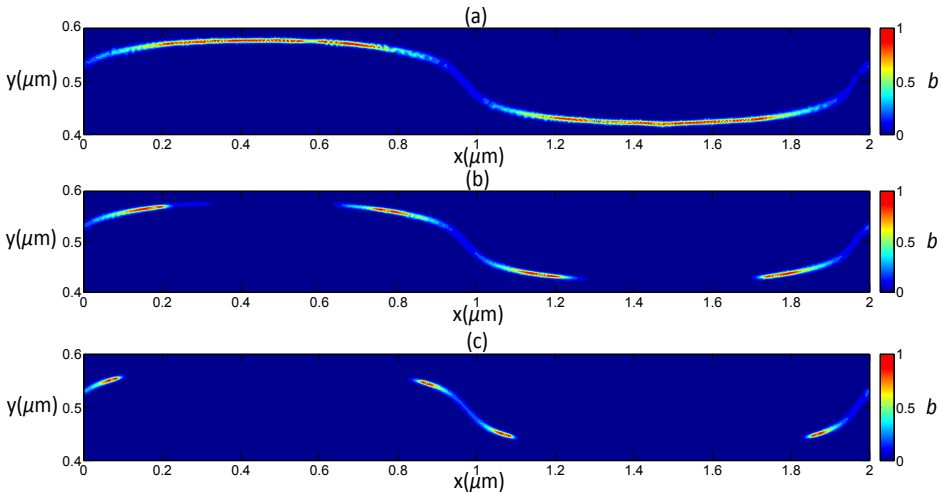
Director field after $15.5\mu\text{s}$



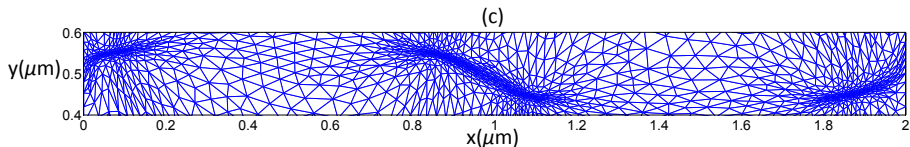
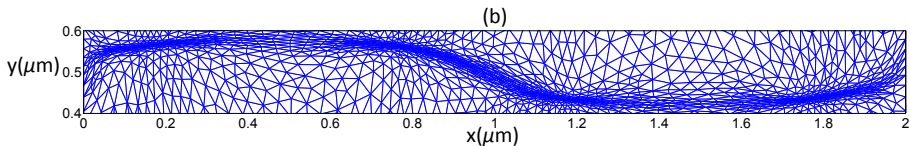
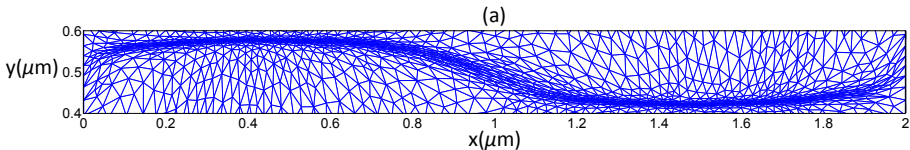
Order parameter S after (a) $15.5\mu\text{s}$ (b) $16\mu\text{s}$ and (c) $17\mu\text{s}$



Biaxiality after (a) $15.5\mu\text{s}$ (b) $16\mu\text{s}$ and (c) $17\mu\text{s}$



Adaptive mesh after (a) $15.5\mu\text{s}$ (b) $16\mu\text{s}$ and (c) $17\mu\text{s}$



Summary and future work

- We have developed a new efficient **moving mesh method** for **Q**-tensor models of liquid crystal cells.
- We have shown that **biaxiality** is a good choice for the monitor input function.
- We demonstrated **optimal** spatial convergence for a model of a static $+1/2$ defect.
- We resolved the movement and core details of **defects** in a time-dependent Pi-cell problem.
- Modelling the creation and annihilation of **moving singularities** on very small length and time scales is a real challenge for numerical methods.
- Future challenges involve the extension to three dimensions and more irregular geometries (e.g. the ZBD).